

## IV - Motors

### 3-phase motors

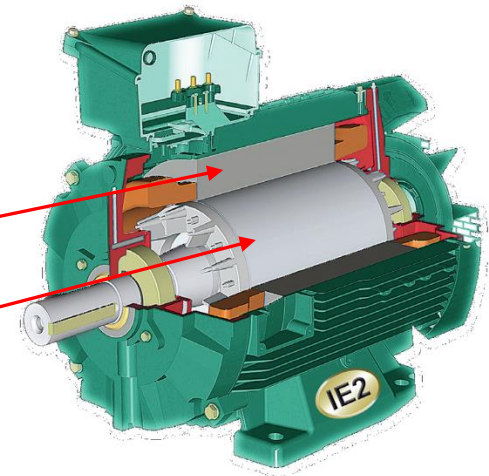
#### - Construction:



DC rotor

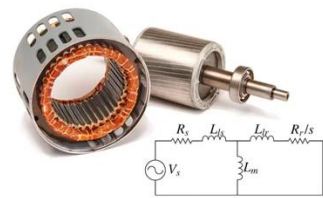
=> Synchronous machine

3-phase  
STATOR  
+  
ROTOR



3-phase rotor

=> Induction/Asynchronous machine



## IV - Motors

### 3-phase motors

#### - The 3-phase stator:

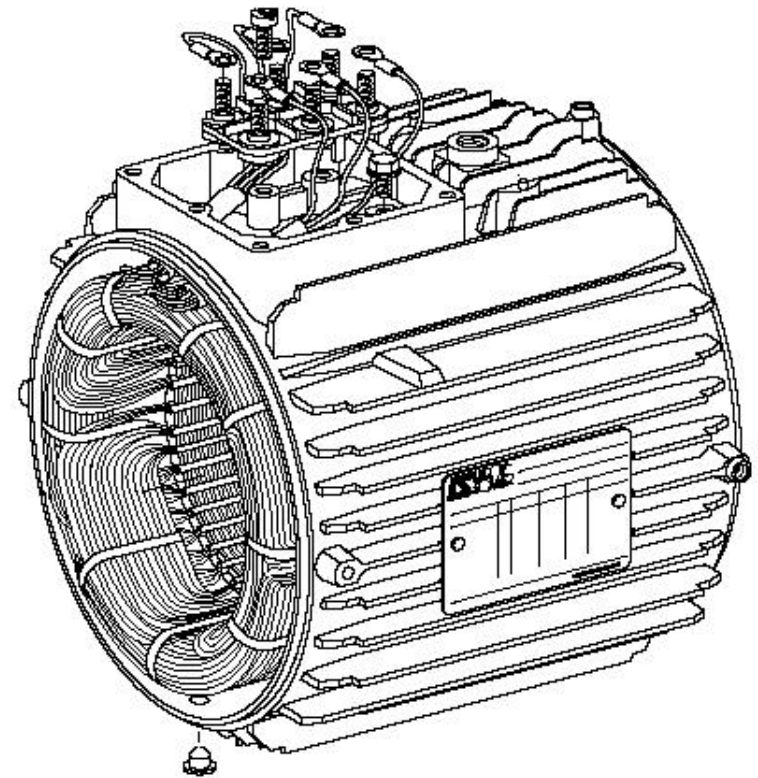
- The stator is the same for both the synchronous and the asynchronous machines

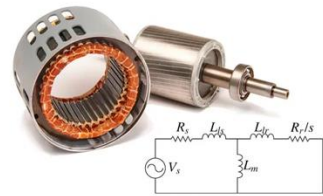
- Consists of an aluminum frame onto which a crown of notched **steel sheets** is fixed.

- Windings of appropriate cross-sections are distributed in these slots, forming a winding assembly with as many circuits as **supply phases** (3).

⇒ **Spatial distribution** of the sinusoidal field

⇒ Creation of a **rotating** magnetic field

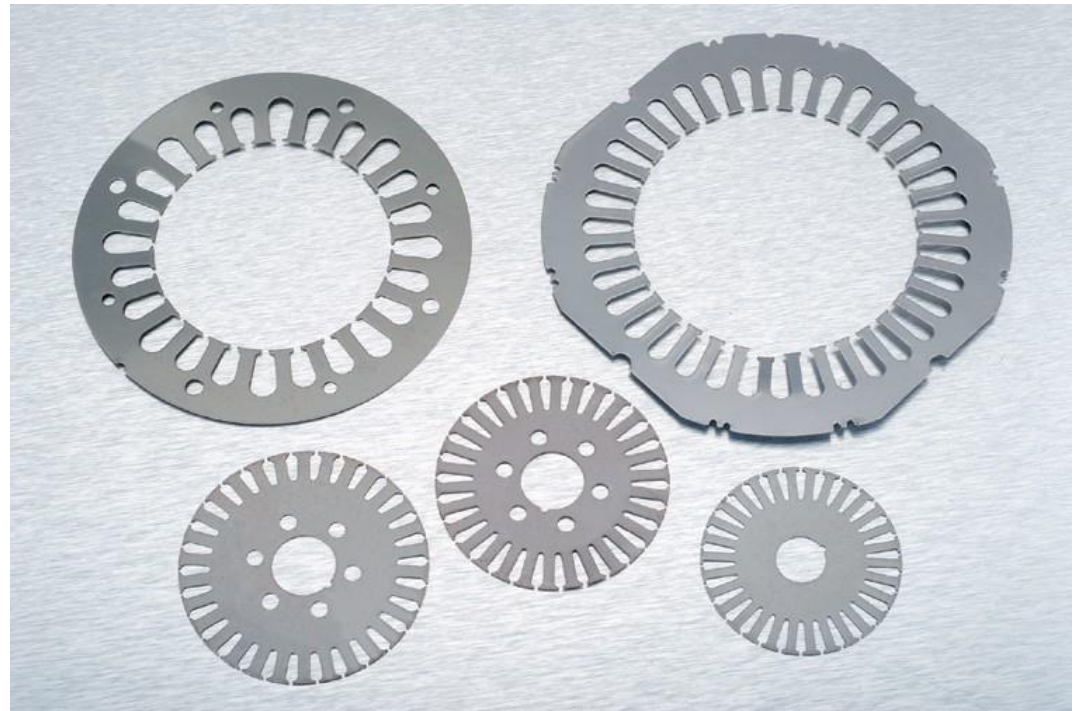




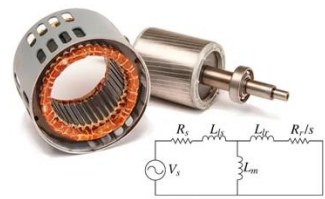
## IV - Motors

### 3-phase motors

#### - The 3-phase stator:



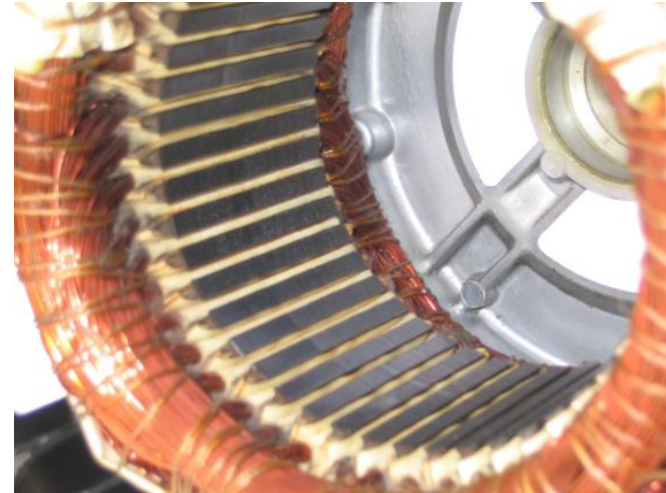


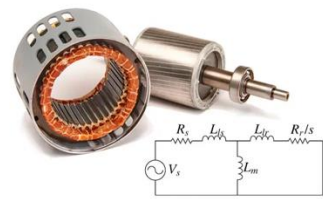


## IV - Motors

### 3-phase motors

#### - The 3-phase stator:





## IV - Motors

### 3-phase motors

- Stator: field distribution

- Field created in an **air gap** by one or several turns

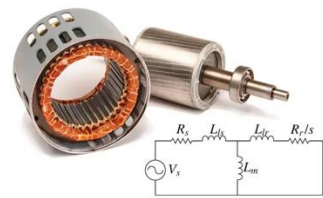
=> **N turns winding arranged in slots** on the surface of an air gap, without leakage, through which flows a direct current  $I$

=> The **iron frame** channels the field lines. In the air gap, there is a  $B$  field that is assumed to be radial.

=> **Conventions**: North pole axis = angular abscissa

=> **Conventions**: Field counted positively when oriented towards the outside of the machine (north pole) and negatively towards the inside (south pole)

=> **Conventions**: Unsaturated magnetic material

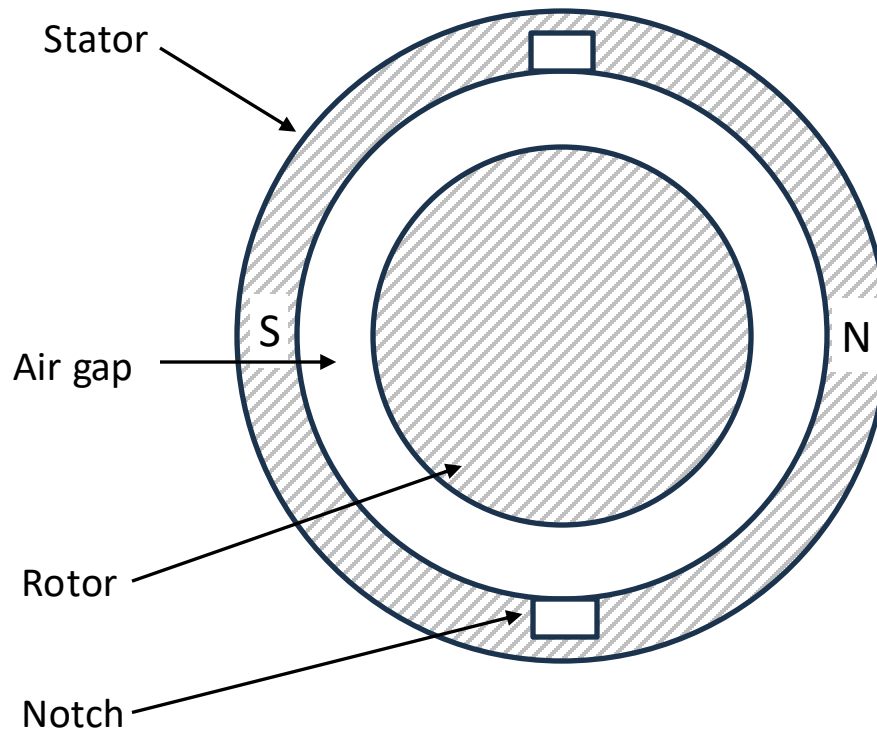


## IV - Motors

### 3-phase motors

#### - Stator: field distribution

- Field created in an air gap by one or several turns: case of the **bipolar stator** + 2 notches



- Ampere's theorem:

$$H_{iron}l_{iron} + H_{air}l_{air} = \sum i_{interlaced}$$

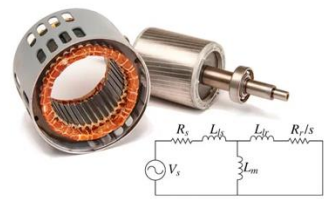
- Assumption of perfect magnetic material

$$\Rightarrow \mu_r \rightarrow \infty \quad \Rightarrow \quad H_{iron} \rightarrow 0$$

- Induction magnetic field in the airgap:

$$B_{air} = \mu_0 \frac{ni}{2e}$$

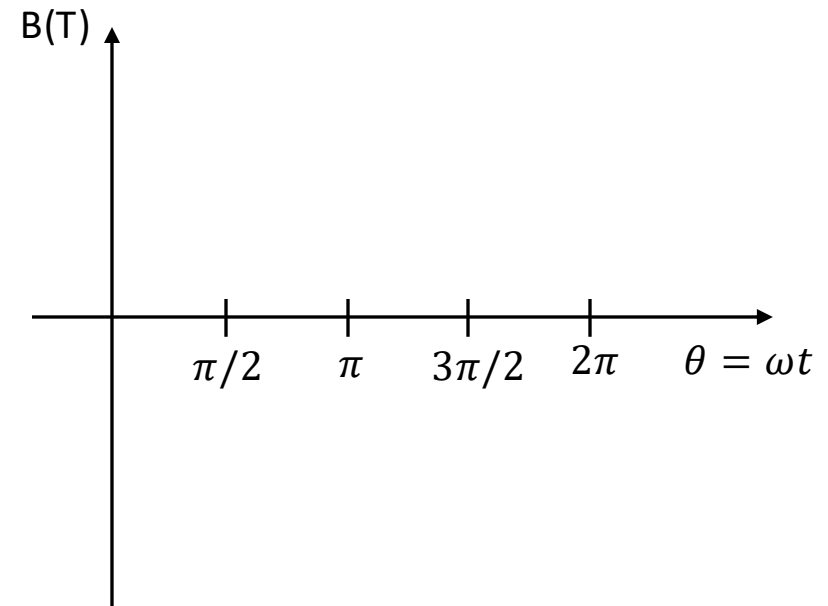
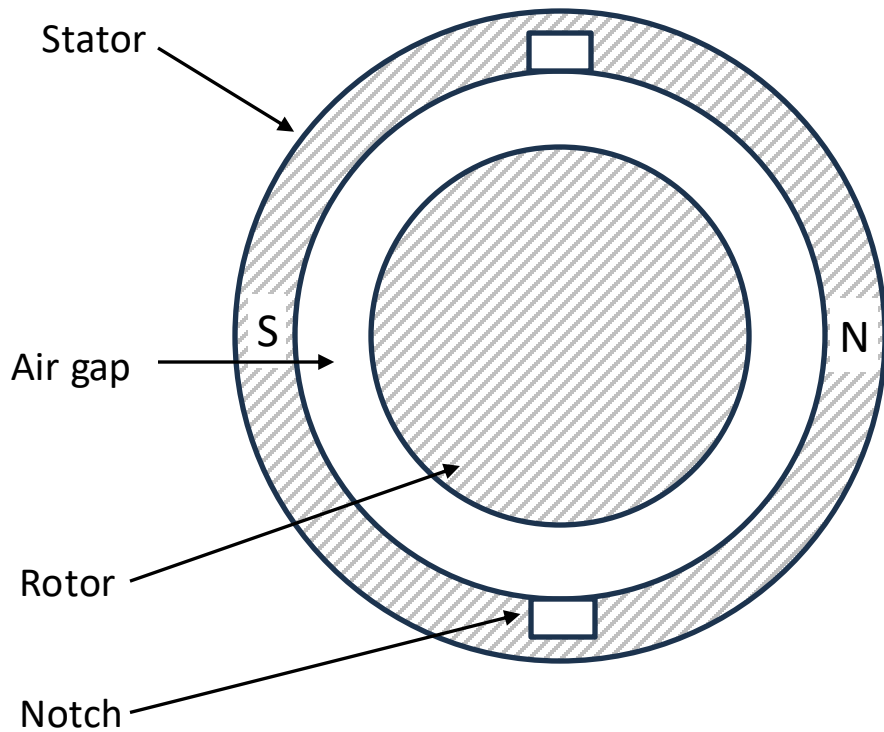
n number of turns, e airgap width

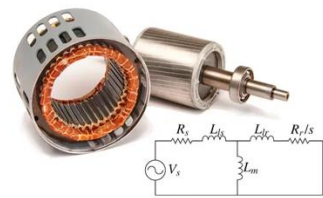


## IV - Motors

### 3-phase motors

- [Stator: field distribution](#)
- Field created in an air gap by one or several turns: **case of the bipolar stator + 2 notches**



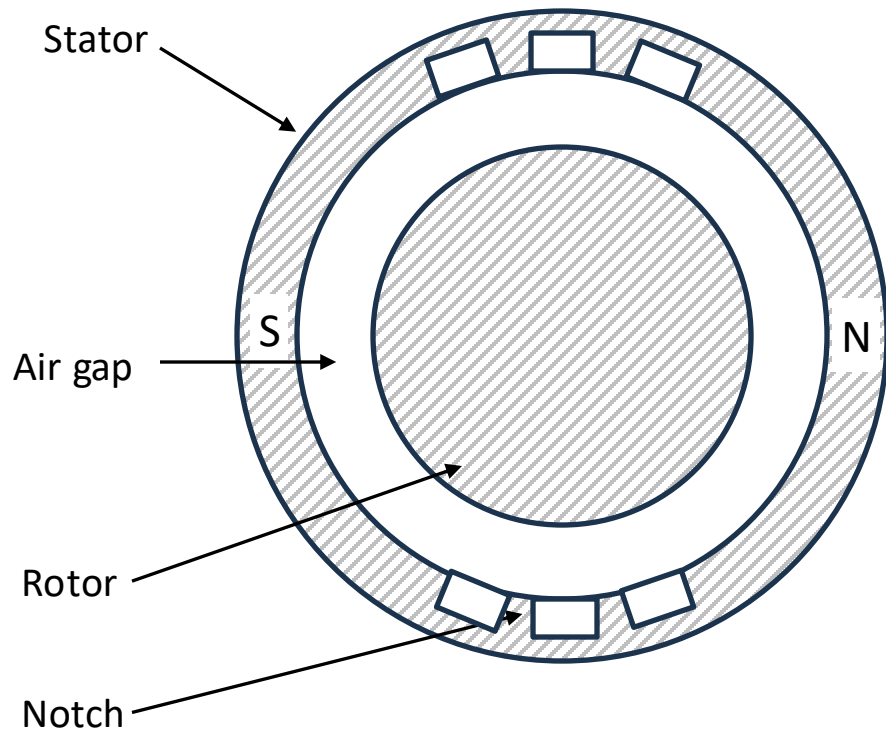


## IV - Motors

### 3-phase motors

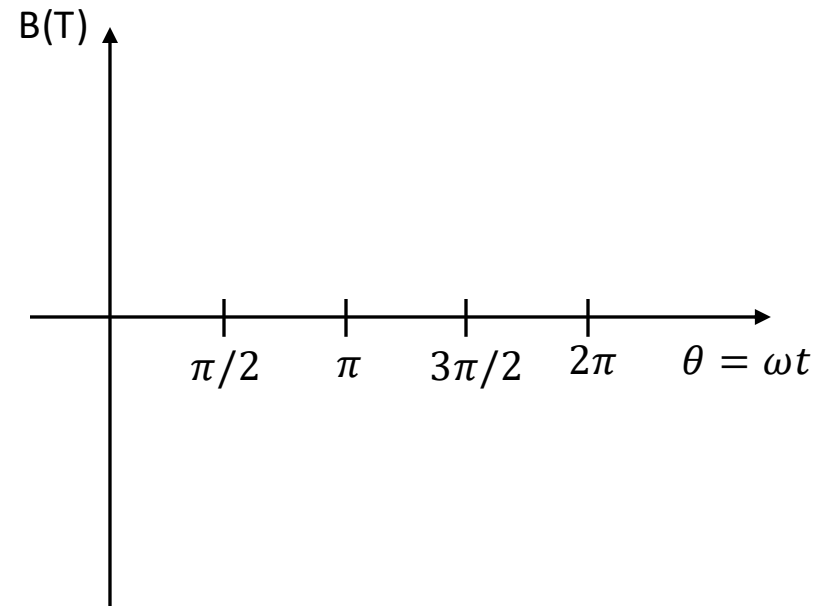
- Stator: field distribution

- Field created in an air gap by one or several turns: **case of the bipolar stator + 3 notches pairs**

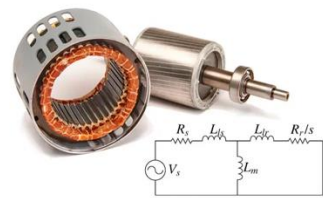


$$B_{air\ 1} = \mu_0 \frac{ni}{2e}$$

$$B_{air\ 2} = \mu_0 \frac{ni}{6e}$$





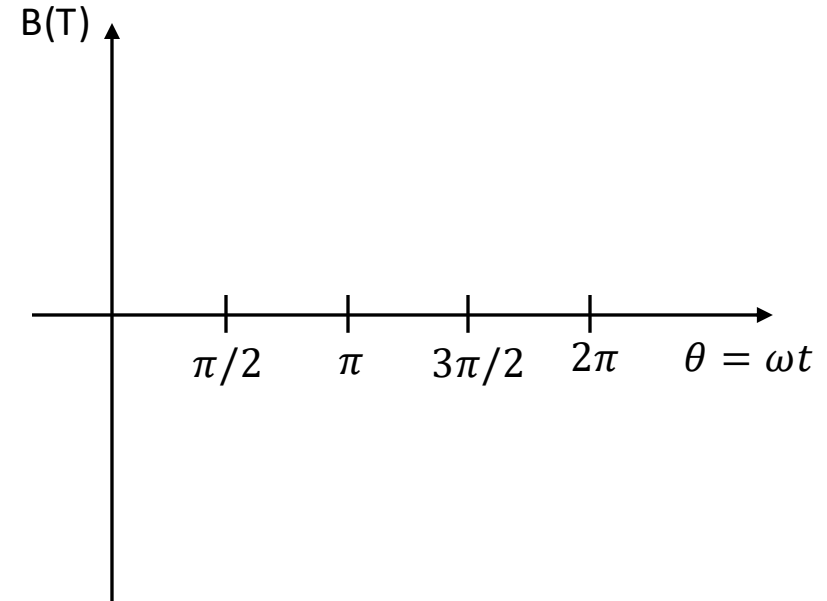
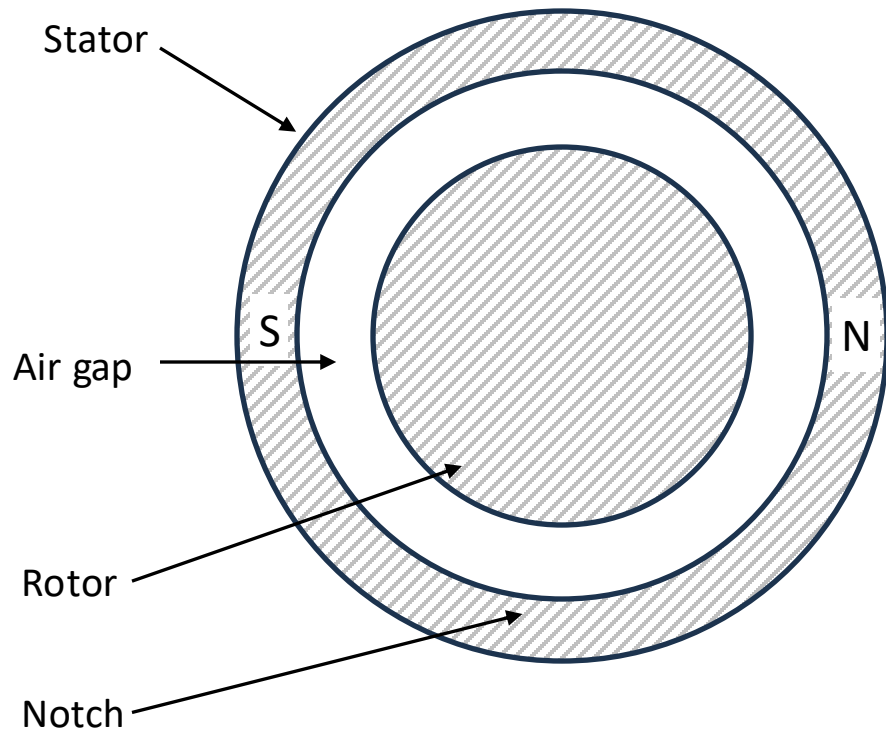


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### 3-phase motors

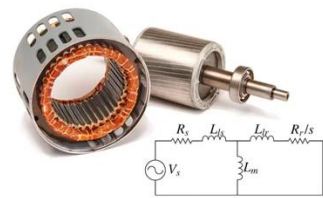
#### - Stator: field distribution

- Field created in an air gap by one or several turns: **bipolar stator** + **notches all around the stator**



=> B field with **sinusoidal spatial distribution**

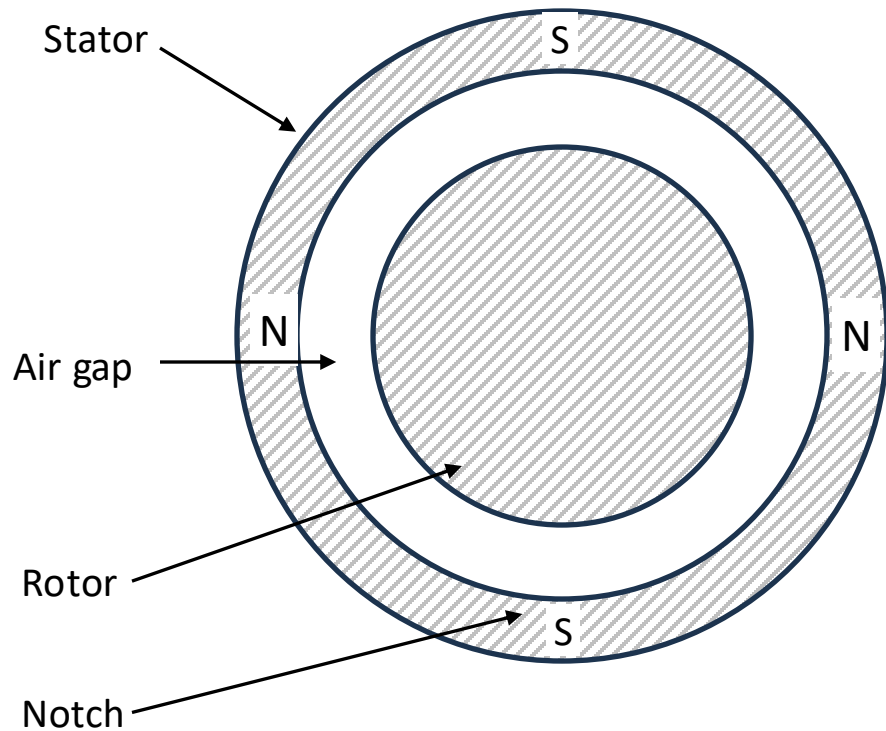
$$B(\theta) = \mu_0 \frac{ni}{2e} \cos\theta = \hat{B} \cos\theta$$



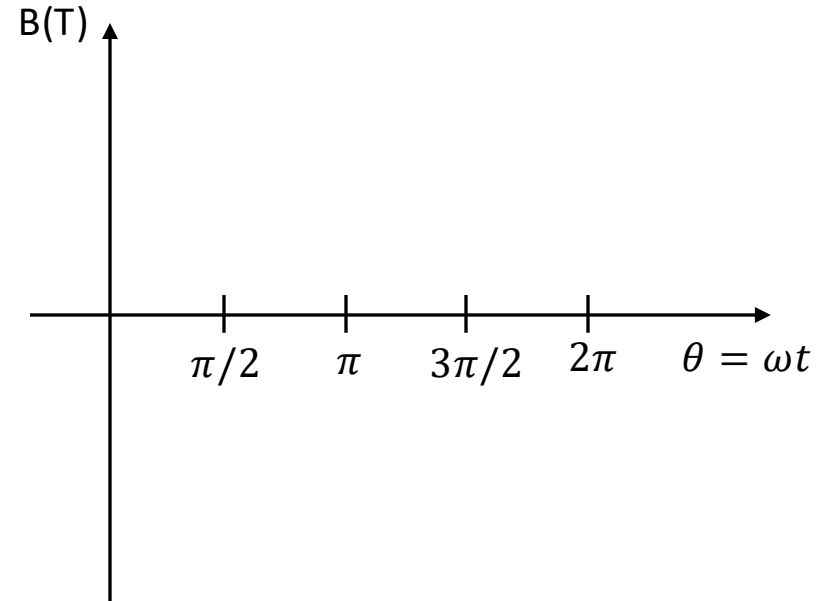
## IV - Motors

### 3-phase motors

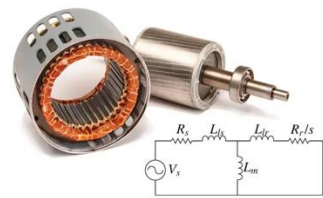
- Stator: field distribution
- Field created in an air gap by one or several turns: **multipolar stator** (**p pole pairs**)



=> Static B field distribution (no rotation)



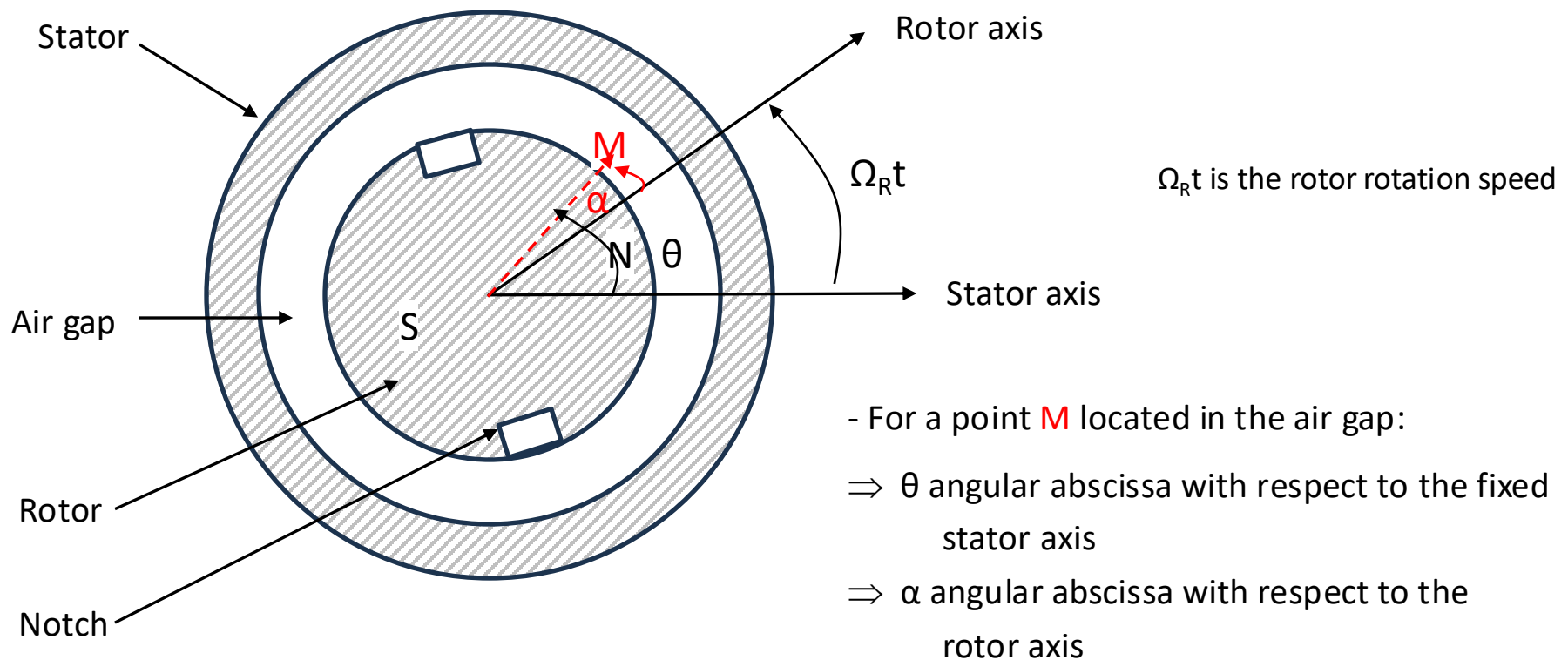
$$B(\theta) = \mu_0 \frac{ni}{2e} \cos p\theta = \hat{B} \cos p\theta$$



## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B field created by a rotor in which a DC current flows: **bipolar rotor**





- Stator: field distribution

- 
- Stator
- Rotor axis
- $\Omega_R t$
- Stator axis
- Air gap
- Rotor
- Notch
- $\theta$
- $\alpha$
- $M$
- N
- S
- The rotor
- $B$

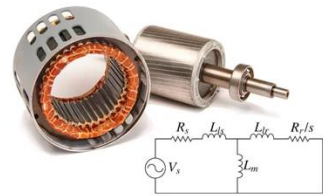
$$\theta = \omega t + \alpha$$

- The rotor winding creates at point M:

$$B(\theta, t) = \hat{B} \cos(\theta - \omega t)$$

=> At a fixed point, it can be observed a  $B(t)$  field varying sinusoidally with time

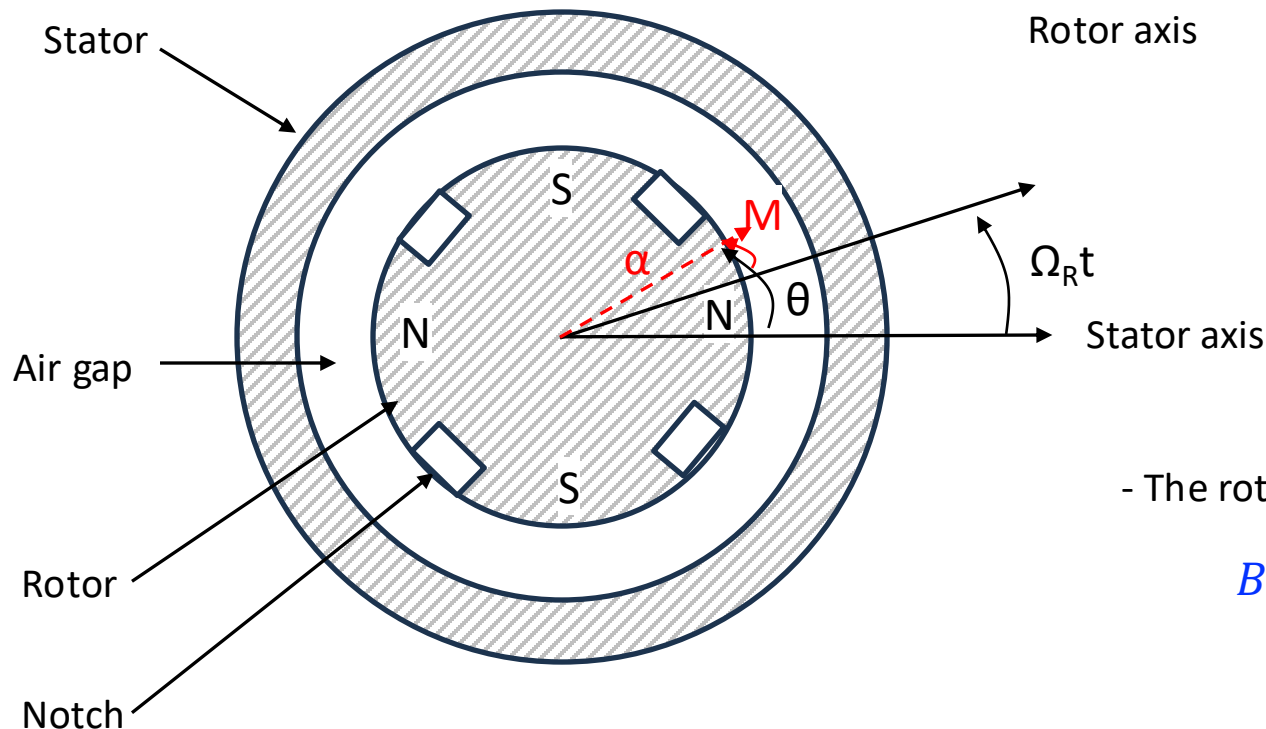
=> At a fixed point and time  $t$ , a static  $B(\theta)$  distribution is observed => rotating distribution field



## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B field created by a rotor in which a DC current flows: **multipolar rotor**



M sees the B field rotating at  
 $\Omega_R = \omega/p$

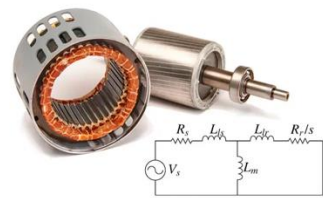
$$\theta = \frac{\omega}{p}t + \alpha$$

- The rotor winding creates at point M:

$$B(\theta, t) = \hat{B} \cos(p\theta - \omega t)$$

=> Sinusoidal distribution of rotating B field

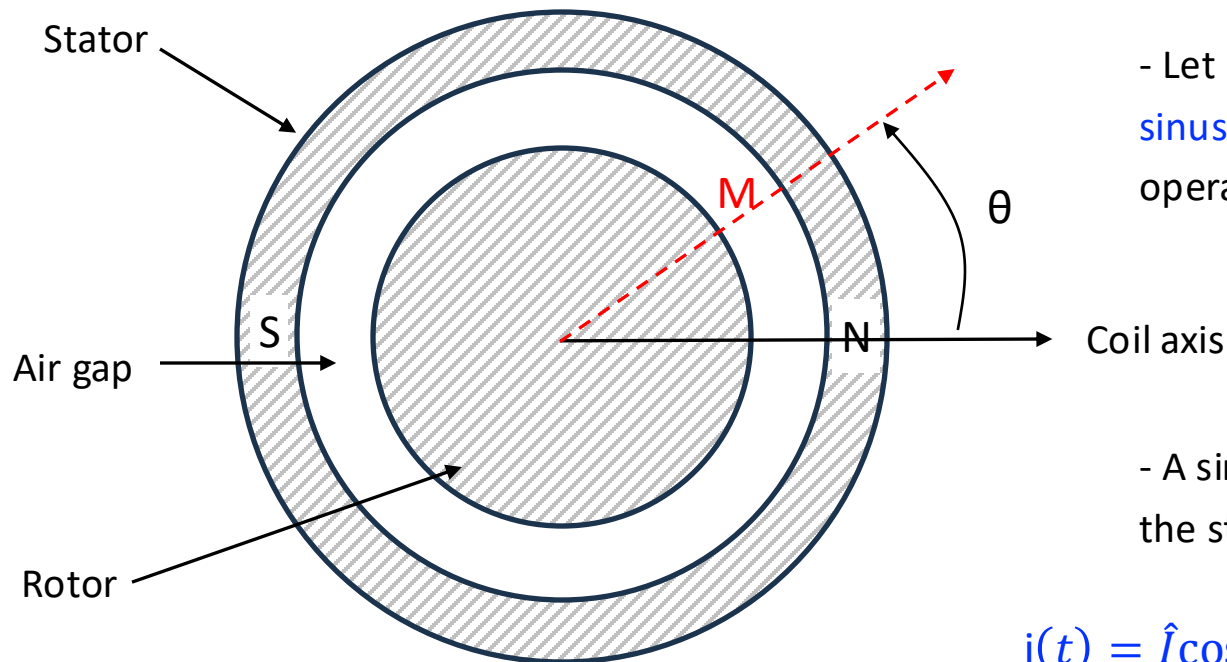




## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B fields created by a **single-phase stator** in which an AC current flows: **bipolar stator**

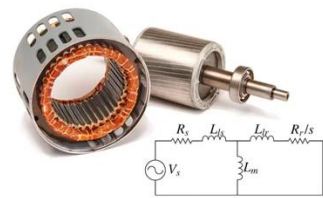


- Let us consider a stator with **sinusoidal spatial distribution** operating in unsaturated mode regime

- A sinusoidal current flows through the stator winding

$$i(t) = \hat{I} \cos(\omega t)$$

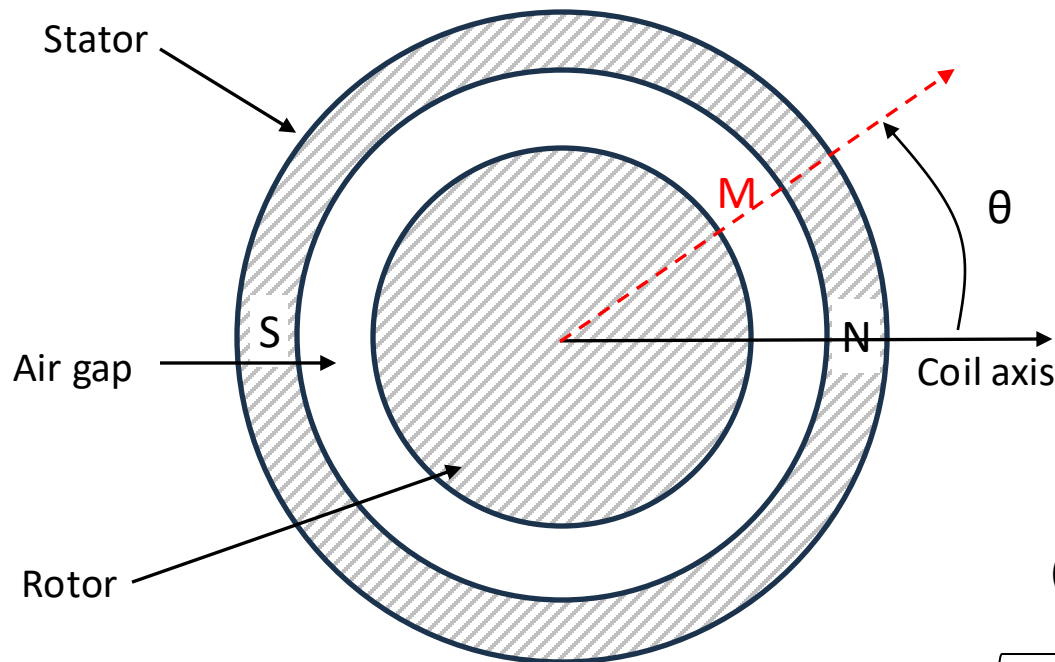
$$B(\theta, t) = k \cdot i(t) \cos(\theta)$$



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- Stator: field distribution
- Rotating B fields created by a **single-phase stator** in which an AC current flows: **bipolar stator**

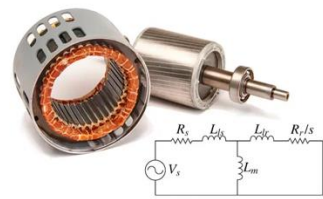


- The winding creates **2 rotating fields** of same amplitude, with sinusoidal spatial distribution, **rotating in opposite directions** at the same speed.

$B_d$   
(direct field)

$B_i$   
(indirect field)

$$B(\theta, t) = \frac{1}{2} k \hat{I} \cos(\theta - \omega t) + \frac{1}{2} k \hat{I} \cos(\theta + \omega t)$$



## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B fields created by a **single-phase stator** in which an AC current flows: **multipolar stator**

#### => Leblanc's theorem

- A fixed, single-phase, **p-polar** stator with sinusoidal spatial distribution, through which flows a sinusoidal current of pulsation  $\omega$  leads to **two rotating fields** (direct and inverse):

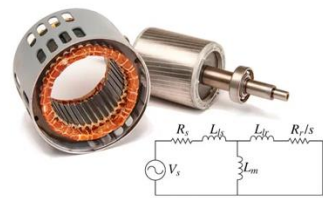
=> Of same amplitude, with sinusoidal spatial distribution

=> Turning in **opposite directions** to each other at rotation speed  $\Omega_s = \frac{\omega}{p}$

=> whose axes coincide with the winding axis at maximum current

$$B(\theta, t) = k\hat{I}\cos(\omega t)\cos(\theta)$$

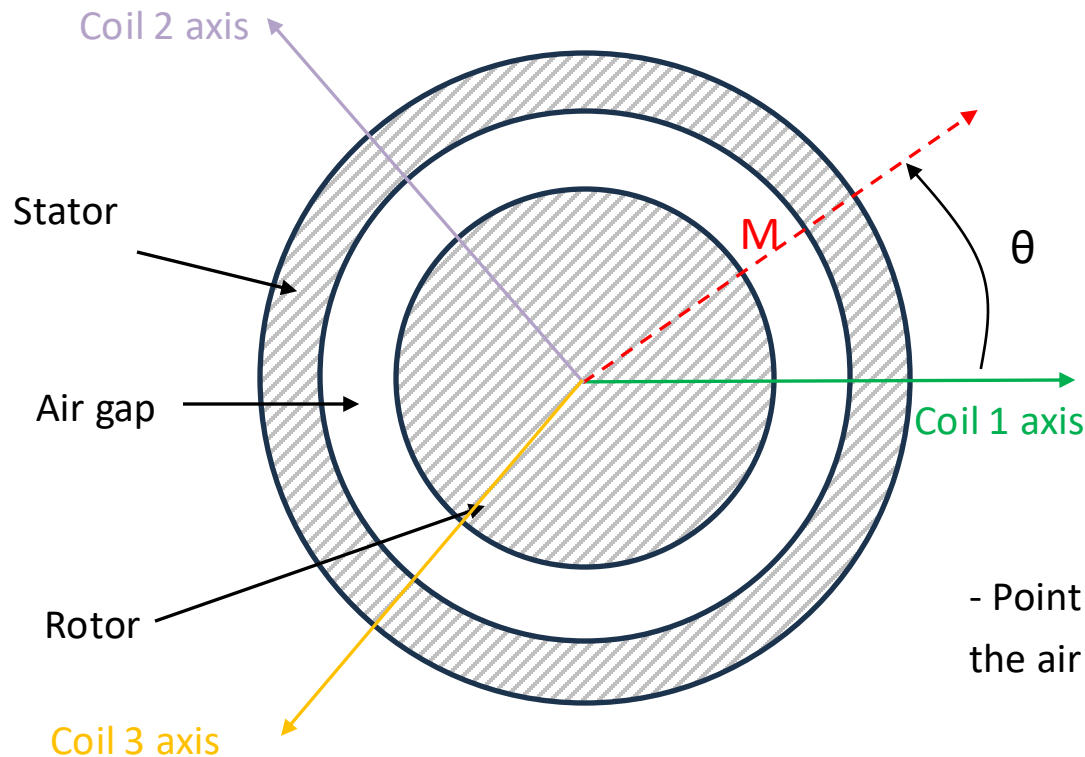
$$B(\theta, t) = \frac{1}{2}k\hat{I}\cos(p\theta - \omega t) + \frac{1}{2}k\hat{I}\cos(p\theta + \omega t)$$



## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B fields created by a **3-phase stator** in which AC currents flow: **bipolar stator**

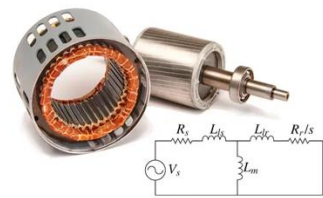


Construction:

- 3-phase winding
- Each coil creates a sinusoidal spatial distribution
- The coil axes are shifted by an angle of  $2\pi/3$ .

- Point **M** located in the air gap at angles:

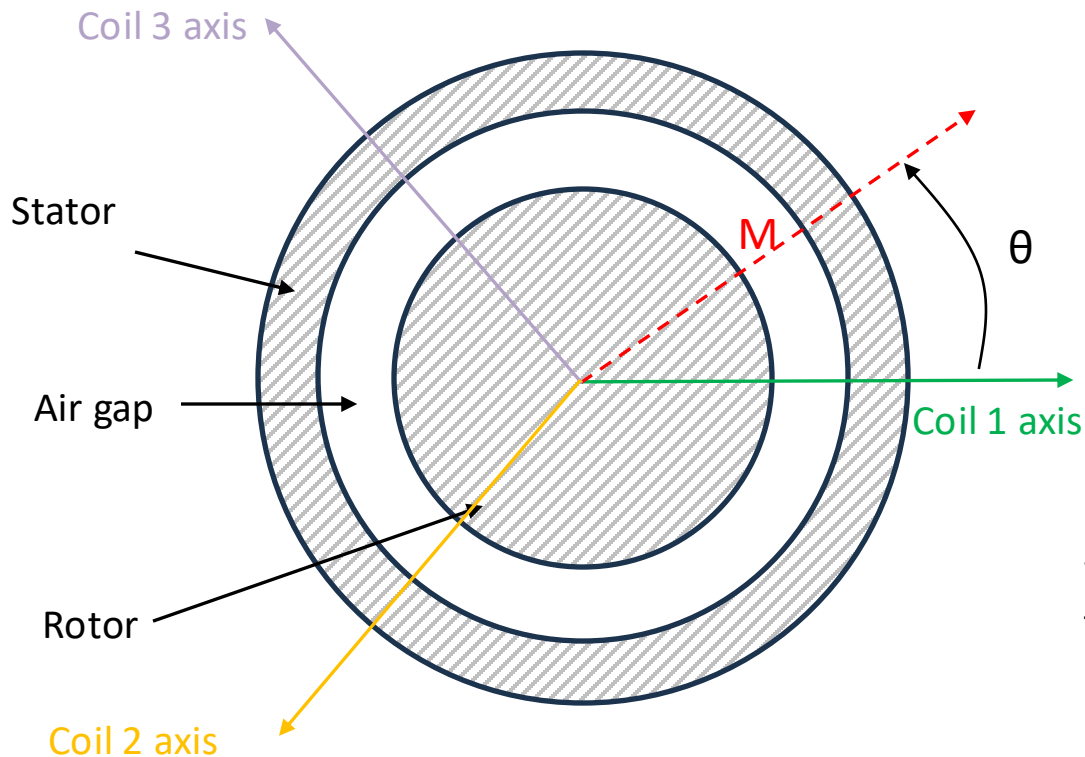
$$\left\{ \begin{array}{l} \theta_1 = \theta \\ \theta_2 = \theta + \frac{4\pi}{3} \\ \theta_3 = \theta + \frac{2\pi}{3} \end{array} \right.$$



## IV - Motors

### 3-phase motors

- Stator: field distribution
- Rotating B fields created by a **3-phase stator** in which AC currents flow: **bipolar stator**



- 3-phase current systems at the windings:

$$i_1(t) = \hat{I} \cos(\omega t)$$

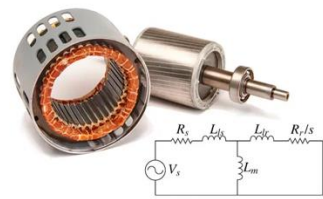
$$i_2(t) = \hat{I} \cos(\omega t - \frac{2\pi}{3})$$

$$i_3(t) = \hat{I} \cos(\omega t - \frac{4\pi}{3})$$

- The resulting B-field is the sum of the fields generated by each winding:

$$B(\theta, t) = \frac{3}{2} k \hat{I} \cos(\omega t - \theta)$$





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- Stator: field distribution

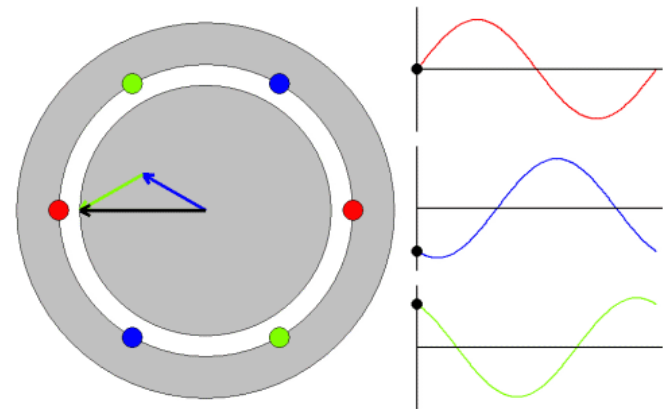
- Rotating B fields created by a **3-phase stator** in which AC currents flow: **multipolar stator**

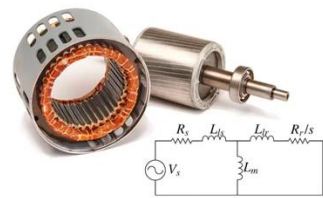
=> Ferraris's theorem

- A fixed, 3-phase, **p-polar** stator with sinusoidal spatial distribution, through which flows a sinusoidal current of pulsation  $\omega$  leads to **one rotating field** (direct and inverse):

=> rotation speed  $\Omega_s = \frac{\omega}{p}$

$$B(\theta, t) = \frac{3}{2} k \hat{I} \cos(\omega t - p\theta)$$

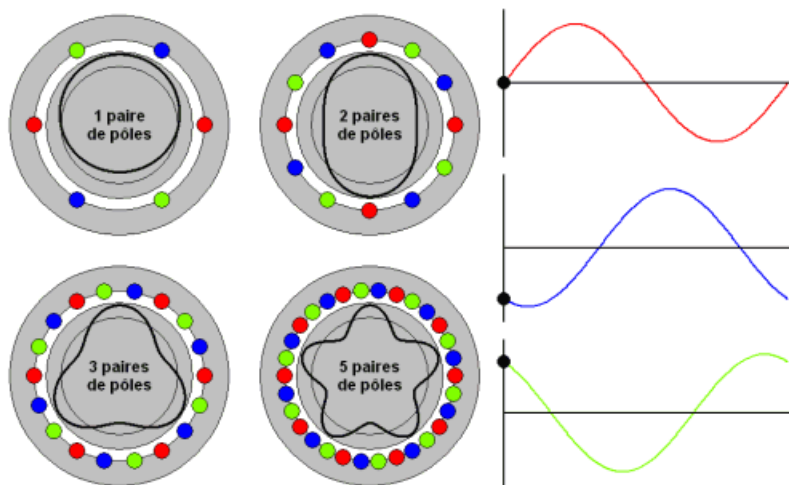




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### 3-phase motors

- Stator: rotating field speed
- Influence of the number of pole pairs (p)



Number of pole pairs	f = 50Hz	f = 60Hz
1	3000 tr/min	3600 tr/min
2	1500 tr/min	1800 tr/min
3	1000 tr/min	1200 tr/min
4	750 tr/min	900 tr/min

NB: Rotation of fields distribution